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(54) Title: METHOD FOR DELIVERING CHEMICALS TO AN OIL OR GAS WELL

(57) Abstract: A method of delivering chemicals to well such as an oil or gas well, the method comprising encapsulating the chemicals in or on a carrier particle such as starch, and delivering the carrier-encapsulated chemical to the well.

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METHOD FOR DELIVERING CHEMICALS TO AN OIL OR GAS WELL

| 1 | |
|-----|--|
| 2 | |
| 3 | This invention relates to a method for encapsulating |
| 4 | chemicals and particularly to a method for starch |
| 5 | and wax encapsulation of aggressive chemicals for |
| 6 | applications in the oil industry. The invention |
| 7 | relates especially to a method of delivering |
| . 8 | chemicals to an oil or gas well, in encapsulated |
| 9 | form. |
| 10 | |
| 11 | Advances in drilling and completion technology have |
| 12 | revolutionized new field development and the use of |
| 13 | sub-sea wells with long tiebacks is now common. The |
| 14 | low temperatures and long fluid transport times |
| 15 | under sub-sea conditions often result in a wide |
| 16 | variety of production chemistry related problems, |
| 17 | including corrosion, scale, wax and asphaltene |
| 18 | deposition, hydrate formation, bacterial growth and |
| 19 | the transport of viscous fluids including emulsions. |
| 20 | The control of these problems is usually achieved by |
| 21 | continuous chemical injection at the sub-sea well |
| 22 | head along separate, multiple injection lines |

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The installation of multiple chemical injection 1 lines is extremely expensive both for subsea 2 wellhead and continuous downhole injection, 3 especially in deepwater environments. 4 5 A deployment method which allowed a reduction in the 6 number of chemical injection lines required to 7 deliver the cocktail of chemicals required at each 8 wellhead would offer significant cost benefits. 9 10 The deployment of combined chemical treatment 11 packages, for example scale and corrosion 12 inhibitors, has been considered as one method of 13 reducing the number of chemical injection lines. 14 This has been achieved on a limited commercial basis 15 by blending selected oilfield chemicals together to 16 form a compatible mixture. However, the development 17 of combined chemical packages is fraught with 18 difficulties due to compatibility issues and is 19 limited to a small range of products and product 20 types. This limits the types of combined treatment 21 available and depending upon the nature of the 22 problem often still results in the use of several 23 injection lines. 24 25 According to the present invention there is provided 26 a method of delivering a chemical to an oil or gas 27 well, the method comprising associating the chemical 28 with a carrier, and delivering the chemical plus 29 30 carrier to the well.

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3 The chemical can be encapsulated by the carrier or 1 otherwise entrapped by the carrier. The carrier 2 preferably comprises a suspension or slurry of 3 particles onto or into which the chemical can be 4 loaded. A typical carrier is particulate starch, 5 but other good carriers can be encapsulating agents 6 conventionally known from e.g. the food, paint and 7 pharmaceutical industries, such as gum arabic, 8 waxes, PVOH, polylactic acids, dextrins, low 9 viscosity modified starches, arabinogalactan, gum 10 acacia, casein, gelatin, carboxymethylcellulose, 11 tragacanth, karaya, sodium alginate, tannin, and 12 13 celluloses. 14 We have found that deploying the chemicals on or in 15 a slurry of nano/micro particles can alleviate 16 compatibility issues during storage and deployment 17 and thus facilitate the injection of multiple 18 chemicals via a single chemical injection line. 19 nano/micro particles can typically contain a high 20 active level of oilfield chemical, typically 5-21 90%v/v, and can be dispersed in either an aqueous or 22 oleic medium, and in solution or suspension, 23 depending upon the nature of the encapsulation 24 25 The entrapped oilfield chemicals are typically released upon contact with the produced 26 fluids due to the breakdown of the coating or 27 carrier matrix either thermally and/or as a result 28

of mixing with oil or water. The potential to

and released along different sections of the

control the rate and extent of release as a function

of time can also allow chemicals to be transported

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pipeline, thus alleviating some of the kinetic 1 2 problems associated with scale, wax and hydrate inhibitors in long subsea tie backs. 3 4 This can enable the simultaneous delivery of 5 combined oilfield chemical packages to platform, 6 remote and complex wells through a single injection 7 The oilfield production chemical-entrapped 8 particles could be injected topsides, at sub sea 9 wellheads or elsewhere in the well. The particles 10 could also be applied to deliver oilfield chemicals 11 that cannot be effectively deployed by conventional 12 solvents. Certain embodiments may include the 13 delivery of a single oilfield chemical to a well 14 while associated with a carrier such as the above-15 mentioned compounds. 16 17 The chemical is typically injected continuously into 18 the well, typically through a dedicated fluid line. 19 20 The nano/micro particle entrapment technology can be 21 applied to deliver a wide range and a wide 22 combination of oilfield production chemicals down 23 one injection line or umbilical. This includes, but 24 is not limited to scale inhibitors, corrosion 25 inhibitors, wax inhibitors, asphaltene inhibitors, 26 hydrate inhibitors, oxygen scavengers, hydrogen 27 sulphide scavengers, demulsifiers, biocides, gel 28 breakers, tracers, friction reducers, surfactants, 29 de-oilers and antifoaming agents. The oilfield 30 chemicals can be entrapped in either liquid or solid 31 32 form.

- 1 The particles can be manufactured using a variety of
- 2 techniques including complex coacervation,
- interfacial polymerisation, desolvation, extrusion,
- 4 agglomeration, emulsion polymerisation, gelation,
- 5 chemical vapour deposition, fluid bed coating, spray
- drying and combinations thereof. The particles can
- 7 be produced over a variable particle size,
- 8 typically, $1\text{nm}-850\mu\text{m}$ and can contain a high active
- 9 level of oilfield chemical, typically 1-90%v/v.
- Nano/micro particles containing different oilfield
- 11 production chemicals can be dispersed into either an
- aqueous or oleic carrier fluid, that may or may not
- contain other oilfield production chemicals, using
- either ionic or non-ionic surface active agents.

 The material is professional.
- The material is preferably stable under injection

 Conditions in bath
- 16 conditions in both aqueous and non-aqueous
- environments at the ambient and sub-ambient
- temperatures that may be encountered in a production
- environment. The entrapped oilfield chemical can be
- 20 rapidly released from the encapsulating and/or
- 21 carrier medium as a result of either thermal
- 22 degradation of the matrix and/or dissolution in
- either the oil or water phase, releasing the
- 24 oilfield chemical under wellhead conditions. The
- release time of the chemical upon contact with the
- 26 produced fluids could also be delayed depending upon
- 27 the nature of the entrapment matrix. This can
- 28 allow chemicals to be transported and released along
- 29 different sections of the pipeline, thus enabling
- 30 the release of chemicals in the right place and
- 31 alleviating some of the kinetic problems associated

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with scale, wax and hydrate inhibitors in long sub 1 2 sea tie backs. 3 The entrapment of certain oilfield chemicals could 4 reduce the corrosivity of the fluid to be deployed 5 into the wellhead or downhole injection system. 6 This could permit the umbilicals and downhole 7 injection lines to be fabricated from lower cost 8 carbon steels rather than the more expensive 9 stainless steels and/or corrosion resistant alloys. 10 11 The particles containing different production 12 chemicals, in either solid or liquid form, can then 13 be mixed together to produce the required blend of 14 oilfield chemicals for dispersion into the fluid 15 carrying medium which may be aqueous or organic 16 The solid particles could be dispersed into 17 the fluid-carrying medium by use of a wide range of 18 different types of amphoteric, anionic, cationic and 19 nonionic surface-active agents. Amphoteric 20 surfactants could include acetates such as lauro-, 21 alkyl- and coco-amphoacetates, betaines such as 22 lauryl-, alkyl- and coco-amidopropylbetaines, 23 glycinates, imidazolines and propionates such as 24 lauro-, alkyl- and coco-aminodipropionate. Anionic 25 surfactants could include alkyl- alkylaryl-, 26 alkylether and alkylarylether sulphonates and 27 carbonates, lignin derivatives, olefine and paraffin 28 sulphonates, phosphate esters and sarcosinates. 29 Cationic surfactants could include amides, amines, 30 amidoamines, diamines and quaternaries such as 31 didecyldimethylammonium. Nonionic surfactants could 32

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- include alkoxylates such as alcohol-, alkylphenol-, 1 2
- amide-, ester-, fatty acid- and glyceride
- 3 ethoxylates, alkylamides, amine oxides and esters.

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- The required dispersing characteristics could be 5
- achieved for example by varying the ratio of a 6
- sorbitan ester and a sorbitan ester ethoxylate to 7
- achieve the desired hydrophilic lipophilic balance 8
- 9 (HLB).

- The chemical is typically coated or otherwise 11
- associated with a carrier such as starch, flour or 12
- wax. The starch can decompose at a given 13
- temperature releasing the chemical at a second 14
- location where it is needed. Selection of the 15
- characteristics of the carrier (e.g. starch) used 16
- allows accurate control over the temperature of 17
- decomposition. Normally the temperature at the 18
- wellhead will be hotter than the surface of the 19
- 20 The precise temperature at the wellhead will
- vary from well to well, and typical subsea wellheads 21
- may have an ambient temperature of around 110°C $\,$ 22
- (compared with 20°C at surface). The starch or wax 23
- coat can typically be designed to decompose when it 24
- crosses a point on the temperature gradient and so 25
- release the chemicals. In particular, wax carriers 26
- can be designed to degrade or dissolve slowly or 27
- after a set time has elapsed to release the 28
- chemicals continuously over a period of time or 29
- 30 after a set interval e.g. in the production fluids.
- 31 The starch or wax may be modified to decompose at
- 32 different temperatures as may be necessary for

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particularly shallow or particularly deep wells or 1 for any other reason in which the temperature of the 2 wellhead may be different from normal. The starch 3 is typically granular starch, and resistant starch 4 made therefrom. The chemical is typically adsorbed 5 onto the starch, typically by simple mixing. 6 Adjuncts useful in controlled release formulations 7 can be added. 8 9 10 All granular starches and flours (hereinafter "starch") may be suitable for use herein and may be 11 derived from any native source. A native starch as 12 used herein, is one as it is found in nature. Also 13 suitable are starches derived from a plant obtained 14 by standard breeding techniques including 15 crossbreeding, translocation, inversion, 16 17 transformation or any other method of gene or chromosome engineering to include variations 18 thereof. In addition, starch derived from a plant 19 grown from artificial mutations and variations of 20 the above genetic composition, which may be produced 21 by known standard methods of mutation breeding, are 22 also suitable herein. 23 24 Typical sources for the starches are cereals, 25 tubers, roots, legumes and fruits. The native 26 source can be corn, pea, potato, sweet potato, 27 banana, barley, wheat, rice, sago, amaranth, 28 tapioca, arrowroot, canna, sorghum, and waxy or high 29 amylose varieties thereof. As used herein, the term 30 "waxy" is intended to include a starch containing at 31 least about 95% by weight amylopectin and the term 32

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"high amylose" is intended to include a starch 1 containing at least about 40% by weight amylose. 2 3 Conversion products which retain their granular 4 structure may be derived from any of the starches, 5 including fluidity or thin-boiling starches prepared 6 by oxidation, enzyme conversion, acid hydrolysis, 7 heat and or acid dextrinization, and or sheared 8 9 products may also be useful herein. 10 Particularly useful are granular structures, which 11 have been "pitted" by the action of enzymes or acid, 12 leaving a still organised structure that creates a 13 microporous starch. The enzymatic or acid hydrolysis 14 of the starch granule is carried out using techniques 15 well known in the art. The amount of enzyme used is 16 dependent upon the enzyme, i.e., type, source and 17 activity, as well as enzyme concentration, substrate 18 concentration, pH, temperature, the presence or 19 absence of inhibitors, and the degree and type of 20 modification. Types of modifications are described 21 herein, infra. These parameters may be adjusted to 22 optimise the nature and extent of the "pitting" of 23 the starch granule. 24 25 Another particulate starch useful in the controlled 26 release applications of the present invention is 27 resistant starch. Resistant starch is commonly 28 known as a starch not likely to be adsorbed in the 29 small intestine of a healthy individual. Granular 30 or particulate starches, such as of the RS2-type (a 31 starch granule that resists digestion by pancreatic 32

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alpha-amylase) and the RS4-type (a chemically 1 modified starch, such as acetylated, 2 hydroxyalkylated, or cross-linked starch) are 3 particularly suitable. However, resistant starches 4 of the RS3-type (retrograded, non-granular starch 5 formed by heat/moisture treatment of starch) are 6 also suitable for the instant invention due to their 7 high level of retrogradation or crystallisation from 8 the alignment and association of associated amylose. 9 10 These types of resistant starch are well known in 11 the art and may be exemplified by that disclosed in 12 US Patent Nos. US 5,593,503 which describes a method 13 of making a granular resistant starch; US Patent 14 Nos. 5,281,276 and 5,409,542 which describe methods 15 of making resistant starches of the RS3 type; US 16 5,855,946 which describes a method of making a 17 resistant starch of the RS4-type; and U.S. 18 Application Serial No. 60/157370, which describes 19 the formation of a very highly resistant starch. 20 The methods for making the resistant starches are 21 described in the preceding references, the 22 disclosures of which are incorporated herein by 23 reference. 24 25 The starch particulate, including granular and 26 resistant starches, may be modified by treatment 27 with any reagent or combination of reagents that 28 contribute to the controlled release properties of 29 30 the starch. 31

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Chemical modifications are intended to include 1 crosslinked starches, including crosslinking the 2 particulate starch with reactive polymers. 3 Preferred reactive polymers include starches 4 modified with aldehyde or silanol groups. Other 5 6 chemical modifications include, without limit, acetylated and organically esterified starches, 7 hydroxyethylated and hydroxypropylated starches, 8 phosphorylated and inorganically esterified 9 starches, cationic, anionic, non-ionic, and 10 zwitterionic starches, and succinate and substituted 11 12 succinate derivatives of starch. 13 Preferred modified starches are starch acetates 14 having a degree of substitution ("DS") of about up 15 to about 1.5, particularly those disclosed in US 16 5,321,132, thereby improving compatibility with 17 synthetic hydrophobic materials. 18 Such modifications are known in the art, for example in 19 Modified Starches: Properties and Uses, Ed. 20 Wurzburg, CRC Press, Inc., Florida (1986). 21 22 Other suitable modifications and methods for 23 producing particulate starches are known in the art 24 and disclosed in U.S. Patent No. 4,626,288 which is 25 incorporated herein by reference. In a particularly 26 useful embodiment, the starch is derivatized by 27 reaction with an alkenyl cyclic dicarboxylic acid 28 anhydride by the method disclosed in U.S. Patent 29 Nos. 2,613,206 and 2,661,349, incorporated herein by 30 reference, or propylene oxide, more particularly by 31 reaction with octenylsuccinic anhydride. 32

| 1 | The encapsulated chemicals can be carried in a |
|----|--|
| 2 | liquid-phase inhibitor or other chemical to be |
| 3 | delivered to the well that may be incompatible with |
| 4 | the encapsulated chemical. All chemicals to be |
| 5 | delivered could then be injected through a single |
| 6 | umbilical. Two umbilicals could be installed to |
| 7 | allow operations to continue in the event of one |
| 8 | blocking up. Additionally a third umbilical for |
| 9 | methanol could be provided. A total of three |
| 10 | umbilicals could therefore provide adequate cover |
| 11 | for a well. This represents a significant saving |
| 12 | when compared with the prior art, which requires |
| 13 | five or six umbilicals for comparable performance. |
| 14 | |
| 15 | Embodiments of the present invention will now be |
| 16 | described by way of example with reference to the |
| 17 | following examples. |
| 18 | |
| 19 | Example 1: Encapsulation of solid material |
| 20 | US Patent 4755397 to Eden et al (incorporated herein |
| 21 | by reference) describes a process for the starch |
| 22 | encapsulation of a solid material, namely, ferric |
| 23 | hydroxide, which can be adapted for the |
| 24 | encapsulation of oilfield chemicals as follows. |
| 25 | |
| 26 | The desired oilfield chemical is dissolved in |
| 27 | acidified water, dilute sodium hydroxide is added as |
| 28 | necessary while stirring to remove from the chemical |
| 29 | any trace precipitates. Ammonium sulphate, water and |
| 30 | high amylose (70%) cornstarch is added to the |
| 31 | chemical slurry to give a slurry of the following |
| 22 | composition: |

| 1 | Starch | | |
|------|-------------------------|------------------|-----------------------------|
| 2 | | 410 grams | (19.9%) |
| | | 610 grams | (29.6%) |
| 3 | Chemical | 41 grams | (2.0%) |
| 4 | Water | 1000 grams | (48.5%) |
| 5 | This slurry is proce | ssed through a | jet cooker (Model |
| · 6 | C-1, National Starch | & Chemical Con | no) at 150°C % |
| 7 | this temperature the | high amylose s | starch cooks |
| 8 | despite the presence | of a high leve | el of an |
| 9 | inhibiting salt, and | forms a unifor | m dispersion a |
| 10 | ball valve attached t | o the outlet o | f the jet socker |
| 11 | can be adjusted so the | at a pressure | drop from months |
| 12 | cooking temperature a | ind pressure to | atmospheria |
| 13 | pressure occurs as th | e starch cook | Oggged +pass=1 |
| 14 | the valve. Upstream | the pressure is | stypicalla |
| 15 | 90psig; downstream th | e pressure is | Typically one |
| 16 | | | oppically opsig. |
| 17 | As the starch passes | through the val | We and the |
| 18 | pressure is reduced to | o atmospheric | its towns. |
| 19 | drops to around 104°C, | the boiling n | Oint of the |
| 20 . | solution at atmospheri | .c pressure 1 | t this |
| 21 | temperature, the starc | h precipitates | e cuts |
| 22 | instantaneously entrap | ping the solid | cssencially |
| 23 | chemical. The product | Collected at | the mark |
| 24 | outlet is typically a | slurry of tan | one cooker |
| 25 | microns in diameter. | The slurry by | variations 5 to 7 |
| 26 | third salt solution and | d two thirds ar | volume, is a |
| 27 | particles. This produc | et is washed for | ecipitated |
| 28 | dried. | To washed II | ee of salt and |
| 29 | | | |
| 30 | The dried particles (40 | la hu mai-le | |
| 31 | various oilfield chemic | ald ame H | ontaining the |
| 32 | synthetic white oil suc | h as Isopar M | exed with a (52% by weight) |

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and a polyalkoxylated alkyl phenol based dispersant 1 (5% by weight) using a high shear, UltraTurrax mixer 2 at 5000 rpm for 10 minutes. A clay based thickening 3 agent (3% by weight) is then added to this mix and 4 blended using a high shear, UltraTurrax mixer at 5 10,000 rpm. 6 7 This process can be used for the production of 8 encapsulated particles containing a) solid biocides; 9 b) de-oilers; c)demulsifiers; d)scale inhibitors; 10 e) corrosion inhibitors; f) wax inhibitors; and 11 g) asphaltene inhibitors. The chemical-loaded 12 particles are mixed in various combinations of 13 chemicals and delivered through a single fluid 14 delivery pipeline to a wellhead, where the 15 temperature of around 110°C breaks down the starch 16 particles and releases the chemicals. Optionally a 17 liquid chemical such as a corrosion inhibitor is 18 mixed with the carrier fluid conveying the particles 19 to the well. 20 21 Example 2: Encapsulation of an Active Ingredient 22 WO9901214 to Fester et al (incorporated herein by 23 reference) describes a process for the encapsulation 24 of an active ingredient, namely, solids and water-25 soluble fluids. This can be adapted for 26 encapsulation of oilfield chemicals as follows. 27 28 Fifteen grams of PN (native potato starch) are added 29 to 100ml water in which 2.5 g Tween 80 is dissolved. 30 Four grams TSTP are dissolved in this suspension, 31 followed by the addition of 20 g of salad oil. An 32

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emulsion forms with the aid of an Ultra-Turrax. 1 The o/w emulsion is then emulsified in a second 2 hydrophobic phase, namely 200ml of paraffin oil. A 3 top stirrer at a speed of 600 rpm is used for this 4 5 purpose. 6 7 A solution of 0.65g NaOH in 10ml water is subsequently added to the emulsion with stirring, in 8 order to initiate partial gelation and cross-9 linking. After 30 minutes, the stirrer speed is 10 increased to 1000 rpm. After 4 hours the emulsion is 11 broken by addition of acetic acid. 12 13 The starch particles collected in the water/acetic 14 acid phase. After separation, the particles are 15 washed with de-ionised water and stored. 16 Examination of the dispersed fluid by light 17 microscopy should indicate that the particles are 18 essentially mono dispersed with a size of 25 μm 19 containing droplets of oil. 20 21 This process can be used for the production of 22 encapsulated particles containing solid and/or 23 liquid chemicals, namely, scale and corrosion 24 inhibitors, oxygen and hydrogen sulphide scavengers, 25 demulsifiers, gel breakers, tracers and antifoaming 26 agents. However, the process could be applicable to 27 any solid or water-soluble chemicals. As before the 28 29 particulate- entrapped chemicals are mixed in various combinations of chemicals and delivered 30 through a single fluid delivery pipeline to a 31 32 wellhead, where the temperature of around 110°C $\,$

| 1 | breaks down the starch particles and releases the | |
|----|---|----|
| 2 | chemicals. Again the liquid phase of the carrier | |
| 3 | fluid can incorporate a further chemical to be | |
| 4 | delivered to the well. | |
| 5 | | |
| 6 | Example 3: Encapsulation of a Water Insoluble Liqu | Lc |
| 7 | US Patent 4755397 to Eden et al (incorporated here | ir |
| 8 | by reference) describes a process for the starch | |
| 9 | encapsulation of a water insoluble liquid, namely, | |
| 10 | peppermint oil, and this can be adapted for the | |
| 11 | production of starch encapsulation of hydrophobic | |
| 12 | oilfield chemicals as follows. | |
| 13 | | |
| 14 | A slurry is made of the following composition: | |
| 15 | High Amylose (70%Corn Starch) 20% | |
| 16 | Ammonium Sulphate 40% | |
| 17 | Water 40% | |
| 18 | | |
| 19 | The following is mixed, to disperse the hydrophobi | C |
| 20 | oilfield chemical and added, with mixing, to the | |
| 21 | previous slurry: | |
| 22 | | |
| 23 | Oilfield chemical 2-10% | |
| 24 | Surfactants 90-98% | |
| 25 | | |
| 26 | The resulting slurry/coarse emulsion is jet-cooked | |
| 27 | through a C-1 cooker as in Example 1. In this case | |
| 28 | the cooker outlet hose empties below the surface of | |
| 29 | a slurry of ammonium sulphate and ice in saturated | |
| 30 | ammonium sulphate solution (-8°C.) to condense and | |
| 31 | trap any free peppermint oil vapours. The resulting | g |
| | amodust is typically soarse (<20 megh) light tan | |

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powder in salt solution. 1 The powder is recovered by 2 filtration and dried. 3 A 3% weight aqueous solution of HEC is then prepared 4 by slowly adding the powdered HEC to distilled water 5 and gradually increasing the mixing speed over a 6 five-minute period. Once a solution is formed a 7 sorbitan ester ethoxylate based dispersant (6% by 8 weight) is added to the aqueous HEC mixture and 9 blended at 2000rpm for five minutes. The dried 10 particles (50% by weight) containing the various 11 oilfield chemicals are then mixed with the aqueous 12 solution of HEC and dispersant using a high shear, 13 UltraTurrax mixer at 5000 rpm for 10 minutes. 14 15 This process is particularly useful for 16 manufacturing encapsulated products containing oil 17 soluble scale and corrosion inhibitors, wax and 18 asphaltene inhibitors, drag reducers, demulsifiers 19 20 and de-oilers. A variety of these chemicals can be encapsulated as described above and delivered to a 21 wellhead via a single injection line in various 22 23 combinations, without interaction between the 24 chemicals in the line during delivery. Upon arrival at the wellhead the starch capsules surrounding the 25 chemicals are broken down by the ambient temperature 26 at the wellhead, and the chemicals are released and 27 activated in situ. Incorporation of incompatible 28 liquid phase chemicals in the carrier fluid does not 29 affect the encapsulated chemical. 30 31

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Example 4: Encapsulation of a solid or oil soluble 1 2 product. US Patent 4997659 to Yatka et al (incorporated 3 herein by reference) describes a process for the 4 encapsulation of a powdered sweetener, namely, 5 Alitame in paraffin and/or microcrystalline wax. 6 This was adapted for the encapsulation of various 7 solid oilfield chemicals as listed above. 8 9 A 20% paraffin or micro-crystalline wax, of defined 10 melting point/80% solid oilfield chemical is 11 prepared by mixing the molten wax with the solid 12 chemical, cooling to form an agglomerate and 13 grinding up the agglomerate to form granules. These 14 granules are optionally further processed to form 15 spheres, using a spheroniser. The size of the 16 spheres is controlled by the granulation process but 17 is typically 1-50 μ m in diameter. 18 19 This process is typically used to produce paraffin 20 or microcrystalline wax-based particles containing 21 solid oilfield production chemicals such as scale, 22 wax and corrosion inhibitors, biocides and other 23 scavengers. In addition the wax particles can be 24 manufactured to entrap oil-based liquids such as 25 corrosion, wax and asphaltene inhibitors, 26 demulsifiers and de-oilers. 27 28 The nano/micro particles containing different 29 production chemicals, in either solid or liquid 30 form, are dispersed together to produce the required 31 blend of oilfield chemicals for dispersion into the 32

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fluid carrying medium which was either aqueous or 1 2 organic based. The solid particles are dispersed into the fluid-carrying medium by use of a wide 3 range of different dispersants. Suitable 4 dispersants include fatty acid esters and 5 alkoxylated (e.g. methoxylated or ethoxylated) fatty 6 acid esters such as sorbitan ester and sorbitan 7 ester ethoxylate; and PEG esters such as PEG 8 laurate. By varying the ratio of the ethoxylated 9 sorbitan ester to the sorbitan ester the desired HLB 10 11 can be obtained. 12 The encapsulated oil field chemicals are mixed in 13 the desired proportions and delivered via a single 14 fluid delivery line to a wellhead, at which point 15 the wax capsules degrade, releasing the chemical 16 into the wellhead environment. Optionally the two 17 or more chemicals that are delivered to the well can 18 be encapsulated by different methods e.g. according 19 to any of the examples herein, so that the different 20 particles release their chemical burdens at 21 different points in the well, in response to 22 23 different stimuli. 24 Example 5: Encapsulation of a wax inhibitor by 25 26 starch. A granular starch (150g, starch octenylsuccinate, 27 aluminum salt, commercially available from National 28 Starch and Chemical Company) was added to a wax 29 inhibitor XPC 3147C (50 g, Aldrich) which had been 30 31 melted at a temperature greater than 30°C. 32 mixture was stirred at ambient temperature and

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pressure in a high shear disperser (Torrence, 1 #785049) at 2000-4000 rpm. An additional 100 g of 2 the granular starch was added to the mixture and 3 stirred for two more minutes to form a fine, free-4 5 flowing powder. This is conveyed to a wellhead as previously described through a single fluid line by 6 a carrier fluid that incorporates a scale inhibitor 7 that is incompatible with the wax inhibitor, without 8 9 any reaction between the chemicals. The scale 10 inhibitor treats the fluid conduit continuously from the point of entry to the wellhead, and the wax 11 inhibitor is activated only after a longer period of 12 time as a result of the starch encapsulating matrix 13 dissolving in the produced fluids. 14 15 Example 6: Encapsulation of a water-soluble chemical 16 17 by starch. Water-soluble solids were formulated with starch at 18 a 1:1 ratio (50% loading on starch). The oil well 19 20 chemical was solubilised in ambient water and homogenised for 1-2 minutes at 9000-10000 rpm 21 (Silverson L4RT). The starch was then added to the 22 solution and the mixture was further homogenised for 23 2-3 minutes at 9000-10000rpm, 20°C (Silverson L4RT). 24 The mixture was spray dried (40% solids, 375°F inlet 25 temperature, 225°F outlet temperature with a feed 26 rate of 160ml/minutes and dual wheel atomisation 27 using Bowen Lab Model (30" x 36") to produce a 28 flowable, non-sticky composition. 29 30 The example was carried out using a scale 31 a.

inhibitor, Scaletreat 2001-28, as the oil well

chemical and Vulca 90, a maize starch 1 crosslinked with 1.5% epichlorohydrin on dry 2 3 starch. The example was carried out using a corrosion 4 b. inhibitor, Corrtreat 2001-29 as the oil well 5 chemical and a starch acetate (1.5 DS) waxy 6 7 maize starch. The example was carried out using a scale 8 c. 9 inhibitor, Scaletreat 2001-26 as the oil well 10 chemical and a microporous waxy maize starch that was digested using 0.3% glucoamylase on 11 dry starch to achieve 15% digestion. 12 13 In each case, the encapsulated chemicals are mixed 14 as desired and delivered in mixtures of encapsulated 15 particles to the well-head through a single fluid 16 The encapsulated particles are degraded by 17 line. the fluid conditions at the well-head, and/or by 18 temperature, thereby delivering their active 19 reagents at the required position in the wellhead. 20 21 Example 7: Encapsulation of a water insoluble 22 chemical by starch. 23 Water insoluble solids were formulated with starch 24 at a 1:1 ratio (50% loading on starch). The oil 25 well chemical was added to a waxy maize starch 26 modified with 3% octenyl succinic anhydride and 27 converted to a water fluidity of 40, and the mixture 28 was homogenised for 1-2 minutes at 9000-10000 rpm, 29 20°C (Silverson L4RT). Water was added to the 30 emulsion and the mixture was further homogenised, 1 31 minute at 9000-10000 rpm, 20°C (Silverson L4RT). 32

22

The starch was then added to the solution and the 1 mixture was further homogenised, 1-2 minutes at 2 9000-10000 rpm, 20°C (Silverson L4RT). The mixture 3 was spray dried (35% solids, 380°F inlet 4 temperature, 230°F outlet temperature, 140-5 160ml/minutes with dual wheel atomisation using 6 Bowen Lab Model (30" \times 36")) to produce a flowable, 7 non-sticky composition. 8 9 a. The example was carried out using a wax 10 inhibitor, Waxtreat 398 as the oil well chemical 11 and a microporous waxy maize which was 30% 12 digested with 0.3% glucoamylase, and modified 13 with 3% octenyl succinic anhydride and 14 crosslinked with 1% aluminium sulphate. 15 b. The example was carried out using an asphaltene 16 dispersant, Waxtreat 7302 as the oil well 17 chemical and a microporous waxy maize starch 18 modified using 3% octenyl succinic anhydride, 19 enzymatically treated using 0.3% glucoamylase, to 20 achieve 30% digestion. 21 c. The example was carried out using a hydrogen 22 sulphide scavenger, Scavtreat 1020 as the oil 23 well chemical and a high amylose corn starch, 24 HYLON® VII starch, commercially available from 25 National Starch and Chemical Company. 26 d. The example was carried out using a kinetic 27 hydrate inhibitor, Hytreat 569 as the oil well 28 chemical and a microporous (30% enzyme digested) 29 waxy maize starch modified using 3% octenyl 30 succinic anhydride, enzymatically treated using 31 0.3% glucoamylase. 32

23 e. The example was carried out using an anti-1 agglomerate hydrate inhibitor, Hytreat A560 as 2 3 the oil well chemical and a cationic starch silanol, 0.3% Nitrogen, 0.4% silanol. 4 5 6 Chemicals are delivered through a single delivery 7 line to a wellhead and also to a well bore and formation. The wellhead chemicals are released from 8 their encapsulated particles at the prevailing 9 wellhead conditions and the formation chemicals are 10 only released upon reaching the more aggressive 11 prevailing conditions at the formation. 12 13 14 Example 8 Starch was weighed out into a glass container. 15 oil well chemical was added while mixing for 5 16 minutes and then mixed for an additional 5 minutes, 17 or until uniform using a Powerstat, Variable 18 Autotransformer set at 80 (3PN168), Bodine Electric 19 Co, Speed reducer motor (NSE-12R). 20 21 a. Starch used was a 50:50 blend of sago and 22 tapioca, DD and the oil well chemical used was 23 Waxtreat 398. The starch:chemical ratio used was 24 25 100:40 and the loading was 28.6%. 26 b. Starch used was a high amylose (70%) maize starch modified by 3% octenyl succinic anhydride and 10% 27 28 polyvinyl alcohol and the oil well chemical used 29 was Waxtreat 398. The starch:chemical ratio used 30 was 100:80 and the loading was 44.4%. c. Starch used was enzyme converted (alpha amylase) 31 maltodextrin and the oil well chemical used was 32

24

Trosquat. The starch:chemical ratio used was 1 100:38 and the loading was 27.5%. 2 d. Starch used was enzyme converted (alpha amylase) 3 maltodextrin and the oil well chemical used was 4 The starch: chemical ratio used was Trosquat. 5 100:38 and the loading was 27.5%. 6 e. Starch used was a high amylose (70%) maize that 7 was gelatinised, completely enzymatically de-8 branched and retrograded and the oil well 9 chemical used was Hytreat A560. 10 starch:chemical ratio used was 100:24 and the 11 loading was 19.3%. 12 13 The encapsulated chemicals are mixed as desired and 14 delivered to production tubing or other well 15 tubulars through a single fluid line. Once reaching 16 the target in the well the chemicals are released 17 through reaction to local conditions. 18 19 The wellhead is the preferred target of the 20 chemicals delivered in order to protect the tie 21 backs etc from corrosion or blockage, but it will be 22 appreciated that the present invention is not in any 23 way limited to the delivery of chemicals to the 24 wellhead, and in certain embodiments the delivery 25 target is another portion of the well, such as the 26 formation, the reservoir, the casing, production 27 tubing or other tubular or conduit. 28 29 Typical embodiments of the invention mitigate 30 compatibility problems with delivery of mixtures of 31 chemicals to platforms, remote and complex wells 32

through a single injection line. Some embodiments 1 also facilitate the deployment of certain chemicals 2 that are difficult to handle, for example, because 3 they are very corrosive and/or are insoluble in 4 conventional solvents; for example, polyacrylate wax 5 6 inhibitors, either alone or in combination with 7 other chemicals, where the chemicals or at least one of them cannot be effectively deployed by 8 conventional solvents. 9 10 Certain embodiments also enable the deployment of 11 oilfield chemicals at high active concentrations, 12 13 for example, ethylene vinyl acetate (EVA) wax inhibitors that cannot be effectively deployed at 14 >10%v/v by conventional solvents. 15 16 While starch is a preferred entrapping or coating 17 medium a range of other materials could be used such 18 as natural gums, cellulose and derivatives, 19 polysaccharides, gelatin, wax, fatty acids, acrylic, 20 carboxyvinyl polymers, polyester, polystyrene, 21 polycaprolactone, polyvinyl acetate, polyamides, 22 polyvinyl alcohol, polylactic acid, polyglycolide, 23 shellac, zein, oil based gels, silica gel and other 24 25 materials consisting of mixtures, copolymers, 26 terpolymers and hydrophobically and/or 27 hydrophilically modified and cross-linked derivatives of the above. 28 29 In certain embodiments the nano/micro particles can 30 31 be dispersed in an aqueous or oleic medium depending

upon the encapsulation matrix, and can contain one

26

or more soluble or dispersed oilfield production

2 chemicals.

3

4 Modifications and improvements can be incorporated

5 without departing from the scope of the invention.

| 1 | Cl | aims |
|----|----|---|
| 2 | 1. | A method of delivering a chemical to an oil or |
| 3 | | gas well, the method comprising associating the |
| 4 | | chemical with a carrier, and delivering the |
| 5 | | chemical and carrier to the well. |
| 6 | | 3.10 WC11. |
| 7 | 2. | A method as claimed in claim 1, wherein the |
| 8 | | chemical is encapsulated by the carrier. |
| 9 | | z zy che carrier. |
| 10 | З. | A method as claimed in any preceding claim, |
| 11 | | wherein the chemicals are released from the |
| 12 | | carrier upon contact with the produced fluids |
| 13 | | in the well. |
| 14 | | |
| 15 | 4. | A method as claimed in any preceding claim, |
| 16 | | wherein two or more chemicals are delivered via |
| 17 | | a single chemical injection conduit. |
| 18 | | J |
| 19 | 5. | A method as claimed in claim 4, wherein the two |
| 20 | | chemicals are mutually incompatible. |
| 21 | | Paradic. |
| 22 | 6. | A method as claimed in claim 4 or claim 5, |
| 23 | | wherein the two or more chemicals are released |
| 24 | | from the carrier at different locations in the |
| 25 | | well. |
| 26 | | |
| 27 | 7. | A method as claimed in any preceding claim, |
| 28 | | wherein the or each chemical is aggressive, |
| 29 | | insoluble or corrosive. |
| 30 | | |

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| 1 | 8. | A method as claimed in any preceding claim, |
|----|-----|---|
| 2 | | wherein the chemical and carrier are carried by |
| 3 | | a fluid to the desired point of delivery. |
| 4 | | |
| 5 | 9. | A method as claimed in claim 8, wherein the |
| 6 | | fluid phase carries a further chemical to be |
| 7 | | delivered to the well. |
| 8 | | |
| 9 | 10. | A method as claimed in claim 8 or claim 9, |
| 10 | | wherein the fluid is aqueous fluid. |
| 11 | | |
| 12 | 11. | A method as claimed in claim 8, or claim 9 |
| 13 | | wherein the fluid is oleic or organic fluid. |
| 14 | | |
| 15 | 12. | A method as claimed in any preceding claim, |
| 16 | | wherein the chemical-bearing carrier is |
| 17 | | injected at surface. |
| 18 | | |
| 19 | 13. | A method as claimed in any preceding claim, |
| 20 | | wherein the chemical-bearing carrier is |
| 21 | | injected at a wellhead. |
| 22 | | · |
| 23 | 14. | A method as claimed in any preceding claim, |
| 24 | | wherein the chemical is selected from the group |
| 25 | | comprising scale inhibitors, corrosion |
| 26 | | inhibitors, wax inhibitors and dispersants, |
| 27 | | asphaltene inhibitors and dispersants, hydrate |
| 28 | | inhibitors, oxygen scavengers, pour-point |
| 29 | | modifiers, hydrogen sulphide scavengers, |
| 30 | | demulsifiers, biocides, gel breakers, tracers, |
| 31 | | friction reducers, surfactants, de-oilers and |
| 32 | | antifoaming agents. |

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29

A method as claimed in any preceding claim, 1 15. 2 wherein the carrier is associated with the chemical by a technique selected from the group 3 4 comprising coacervation, interfacial 5 polymerisation, desolvation, extrusion, 6 agglomeration, emulsion polymerisation, 7 gelation, chemical vapour deposition, fluid bed coating, spray drying and combinations thereof. 8 9 A method as claimed in any preceding claim, 10 16. wherein the carrier is selected from the group 11 12 comprising starch or flour, gum arabic, waxes, PVOH, polylactic acids, dextrins, low viscosity 13 14 modified starches, arabinogalactan, gum acacia, casein, gelatin, carboxymethylcellulose, 15 tragacanth, karaya, sodium alginate, tannin, 16 17 and celluloses. 18 A method as claimed in any preceding claim, 19 17. 20 wherein the chemical is continuously delivered 21 to the well. 22 23 A method as claimed in any preceding claim, 18. 24 wherein the carrier and chemical forms a 25 particle. 26 A method as claimed in claim 18, wherein the 27 19. 28 particle size is in the range of $1\mu\text{m--}20\mu\text{m}.$ 29 20. A method as claimed in any preceding claim, 30

wherein the carrier dissolves into the produced

30

1 fluids from the well after releasing the

2 chemical.

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